

Sequence of Events			Observations
11/8/2021	10:17	GT2 Start Command	
	10:31	GT2 FSNL	
	11:12	Main Steam reached Steam Turbine startup conditions	Ramp rate is too high. In less than one hour, the HRSG reached steam turbine operating conditions. It should have taken 3.5 hours.
	13:21	GT2 Synch - MW setting adjusted from 25 to 16	
	13:24	GT2 - Temp Matching Mode Enabled	
	13:30	CRH condensate drain valve set in Auto mode	
	14:27	GT2 - Temp Matching Mode Disabled	Deviation from startup procedure. Not documented in log book or in the startup procedure record. Plant leadership wanted to lower emissions.
	14:27	GT2 - MW setpoint increased to 90MW	
	14:31	SCR in service	
	14:56	GT2 - Reaches 90MW	Operators questioned plant leadership about running the GT at 90MW and it was decided by plant leadership to leave it at 90MW.
	15:33	STG reset but would not start	Communications failure in the Toshiba DCS, troubleshooting began
11/9/2021	15:33	Troubleshooting efforts into loss of DCS communication with field sensors and devices	
11/10/2021	All Day	Troubleshooting continued, working to get Profibus operating	GT2 - operation remained at 90MW
		Profibus operation restored, DCS communications working	
	13:02	GT2 - MW setpoint decreased from 90MW to 45MW	Operator began lowering the GT to minimize heat input to the HRSG
	13:06	GT2 - MW setpoint decreased from 45MW to 15MW	Operator lowered the GT to its minimum load to minimize heat input to the HRSG
	13:06	STG reset and auto start initiated	
	13:06	Main Steam (1,035F @ 1,369psi)	Design is
	13:06	STG - Cold-Cold Start Condition & Slow startup	
	13:06	STG - 2:1 Flow Control in Service	

Figure 9, Timeline of event (Part 1 of 2)

		Sequence of Events	Observations
11/10/2021	13:08	GT2 - MW setpoint increased from 15MW to 90MW	Operator was instructed by the Operations Manager to raise the MW back up to get into DLN emissions mode
	13:40	GT2 - MW setpoint decreased from 90MW to 50MW	Unclear why the changes in GT MW setpoint
	14:40	GT2 - MW setpoint increased from 50MW to 90MW	Unclear why the changes in GT MW setpoint
	14:50	GT2 - MW setpoint increased from 90MW to 110MW	Unclear why the changes in GT MW setpoint
	14:58	Main Steam (1,042F @ 1,500psi)	Design is [REDACTED]
	15:25	STG - HP Turbine Exhaust Temp High Alarm	[REDACTED]
	15:27	STG - Alarms Acknowledged (this includes the HP Turbine Exhaust Temp High Alarm)	Acknowledgement only, no actions taken by anyone
	15:29	STG - FSNL	
	15:29	STG - 41E Excitation Breaker Failed to Close	Troubleshooting began
	17:20	STG - HP Turbine Exhaust Temp >1120F	Max range of the thermocouple is 1120F
	17:29	STG - HP Inner Casing Upper Metal Temp >1120F	Max range of the thermocouple is 1120F
	17:38	STG - HP Inner Casing Lower Metal Temp >1120F	Max range of the thermocouple is 1120F
	17:47	STG - Exhaust Pressure > 1st Stage Pressure	No flow through the HP
	19:49	STG - 41E Repaired and Closed	Excitation began, unit ready to synchronize.
	19:54	STG - 52G Breaker Fails to Close	Troubleshooting began
	20:44	STG - CRH pipe ruptures	
	20:47	STG - Manually Tripped	
	20:47	GT2 - Manually Tripped	
	23:49	STG - HP Turbine Exhaust Temp <1120F	Max range of the thermocouple is 1120F
11/11/2021	2:32	STG - HP Inner Casing Lower Metal Temp <1120F	Max range of the thermocouple is 1120F
	5:59	STG - HP Inner Casing Upper Metal Temp <1120F	Max range of the thermocouple is 1120F

Figure 9, Timeline of event (Part 2 of 2)

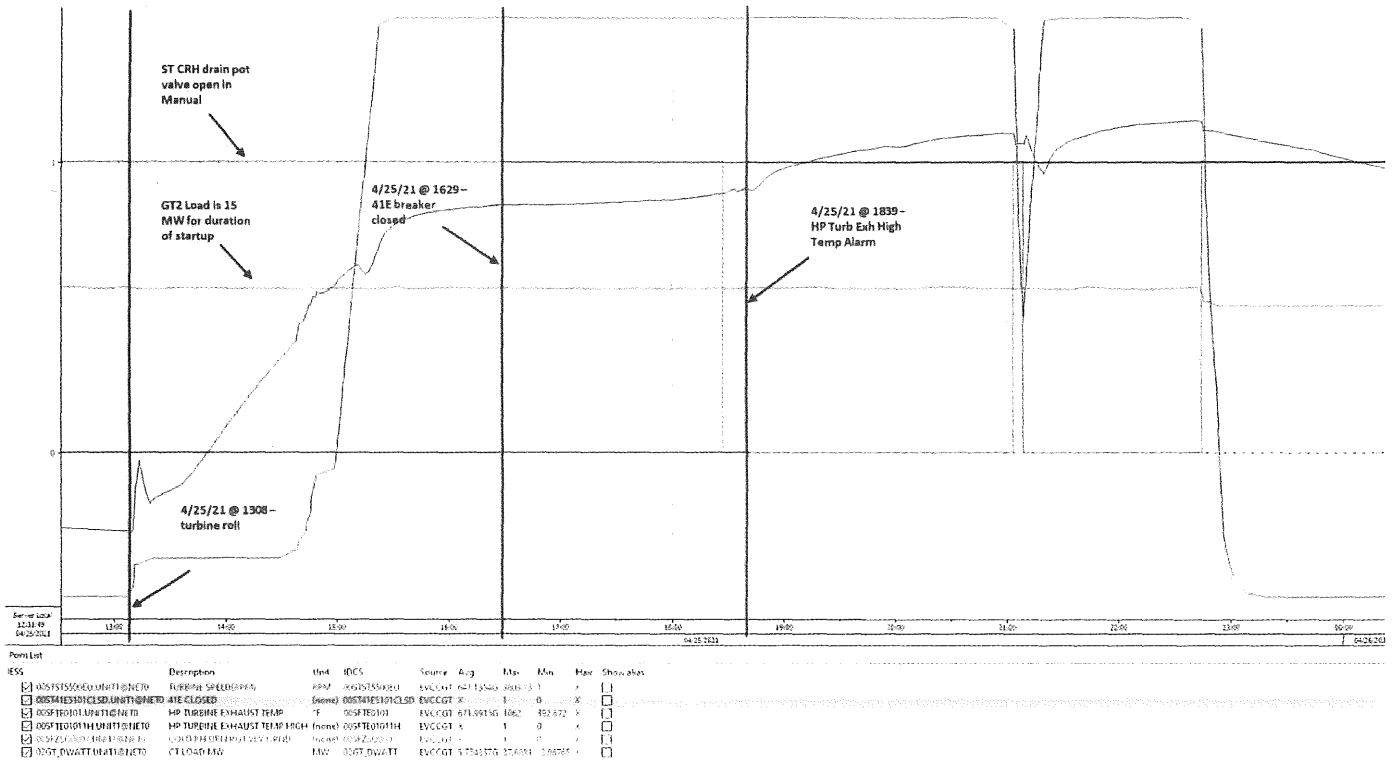


Figure 10, Effect of CRH drain valve on April 25, 2021, STG Startup

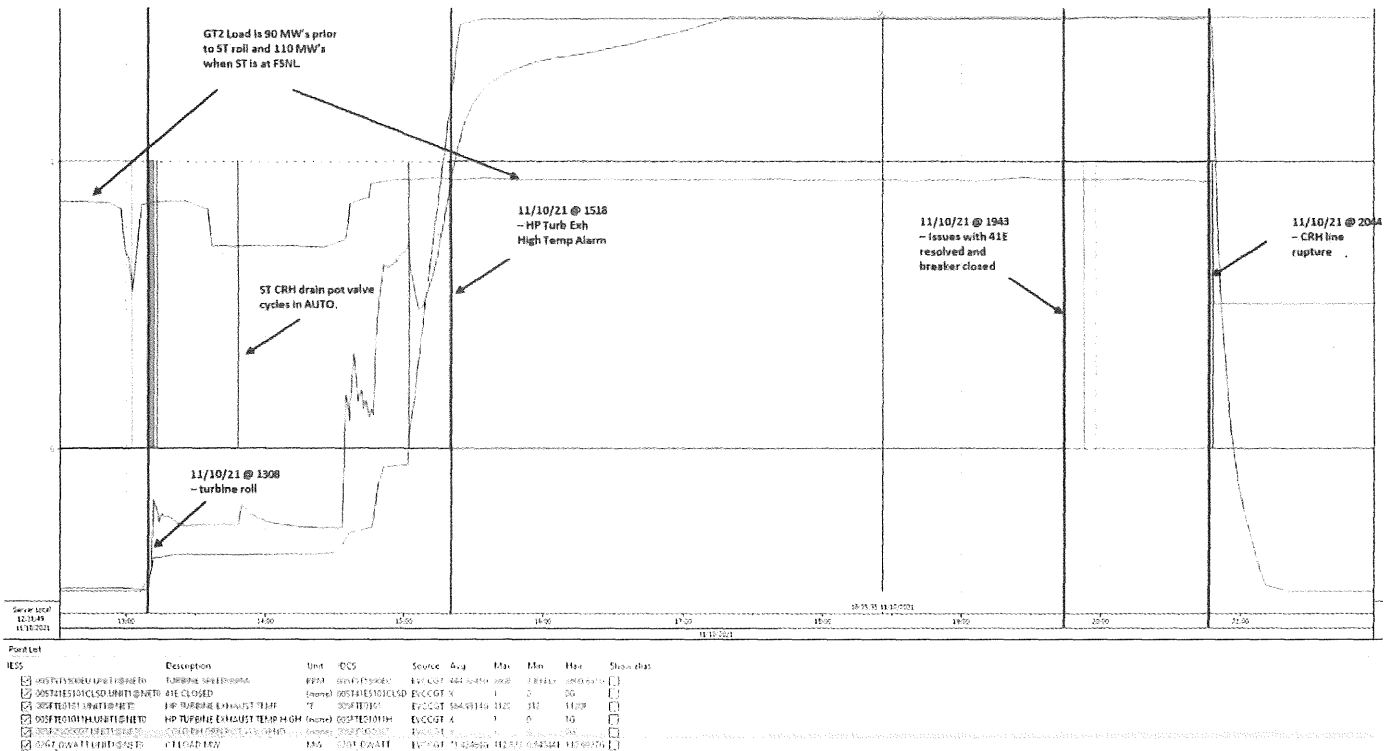


Figure 11, Effect of CRH drain valve on November 10, 2021, STG Startup

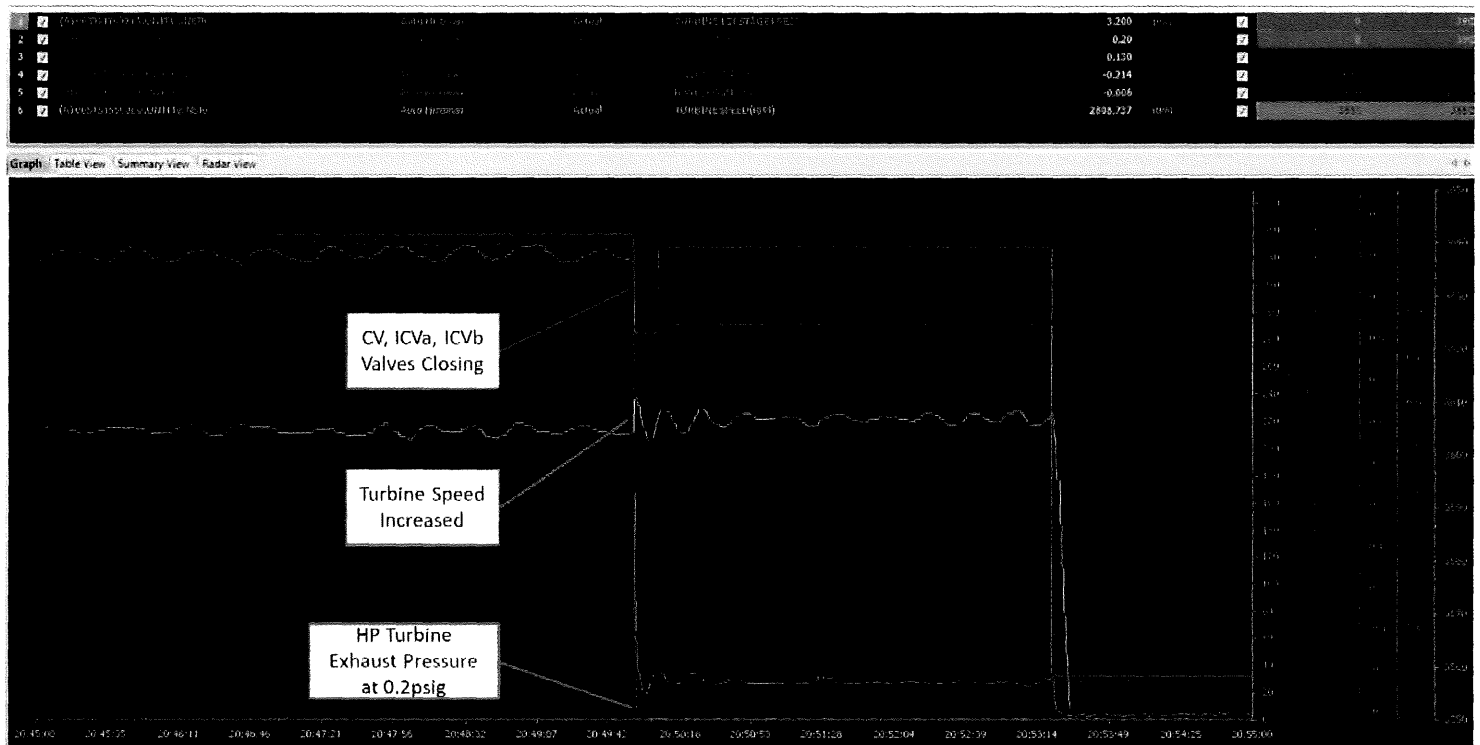


Figure 12, STG Trend data of at time of pipe rupture

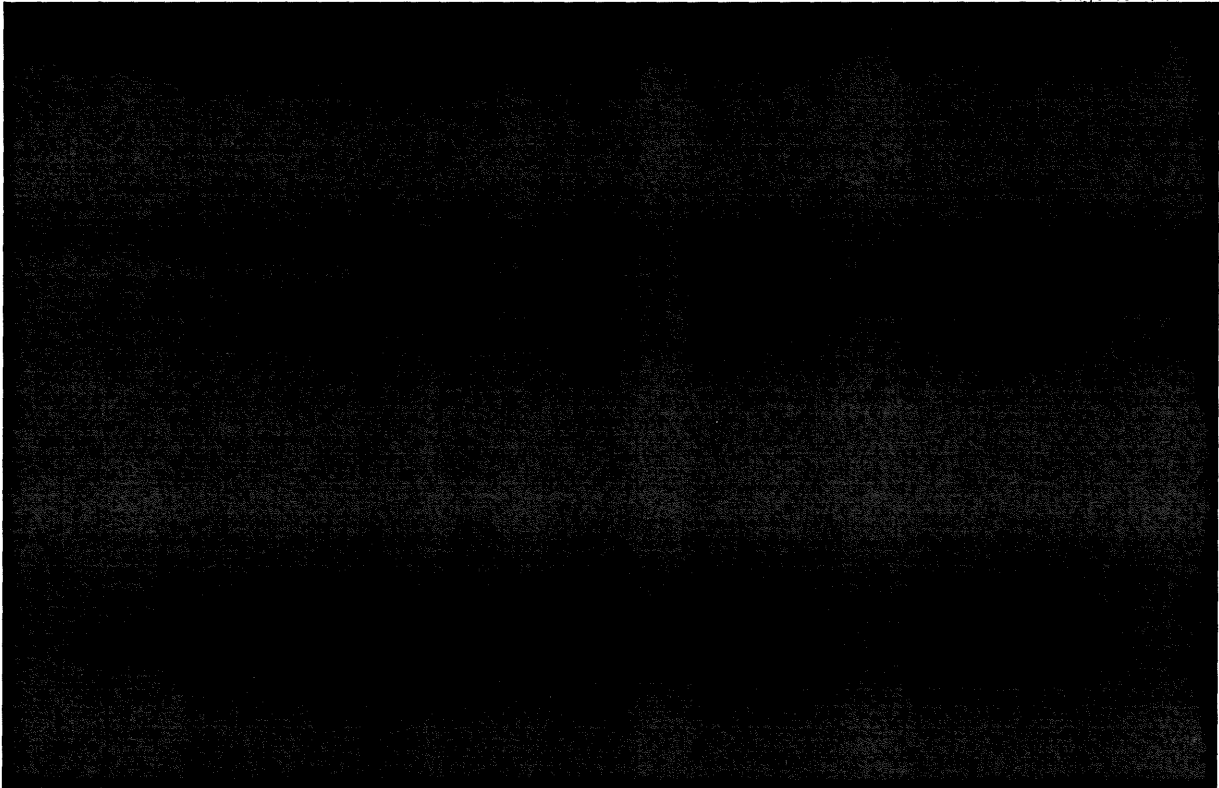


Figure 13, Red Lined DCS drawing of IP Bypass Setpoint control logic

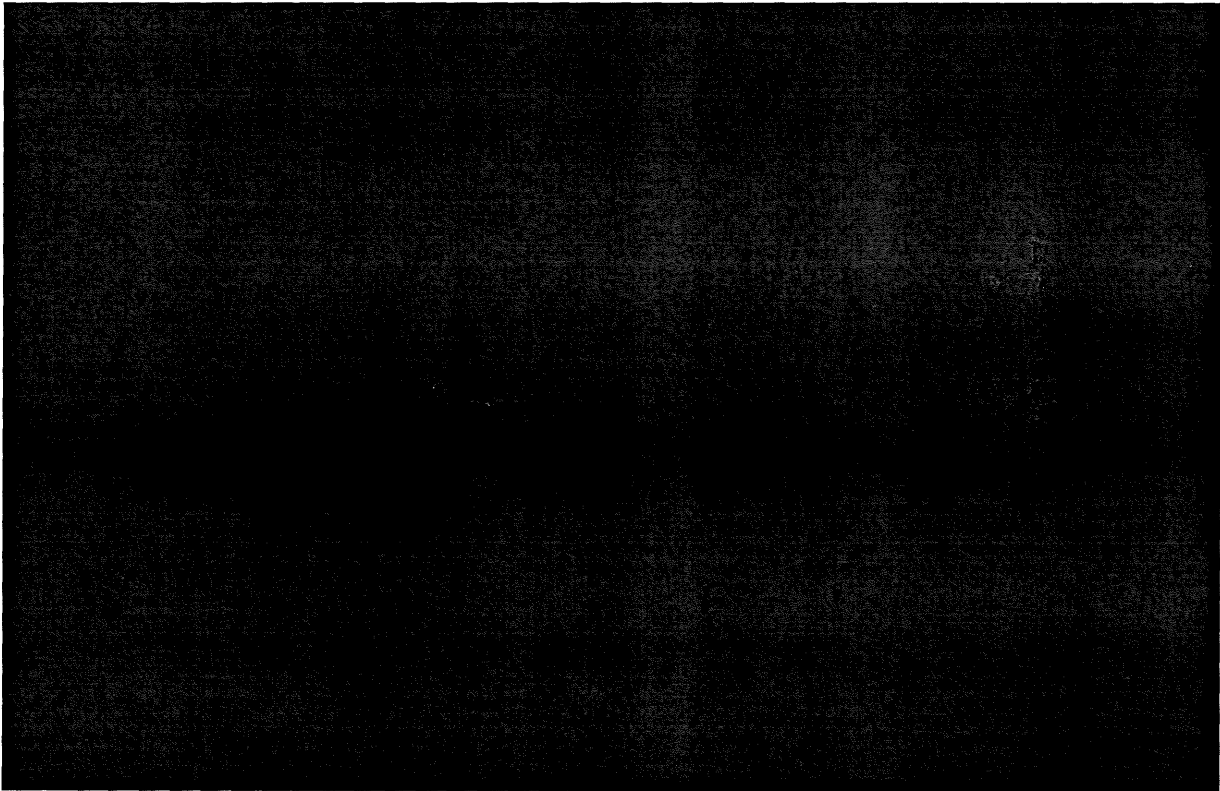


Figure 14, Red Lined DCS drawing of HP Bypass Setpoint control logic

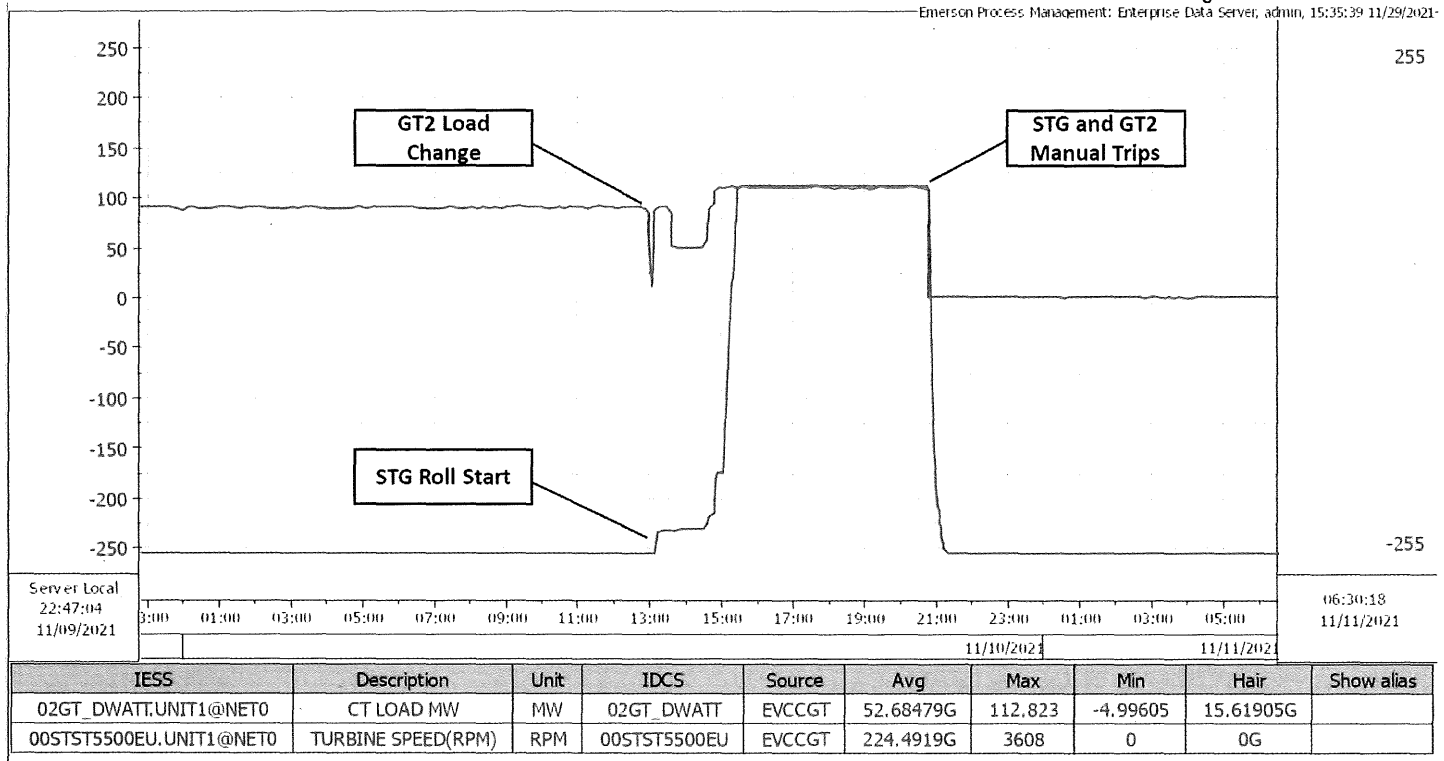
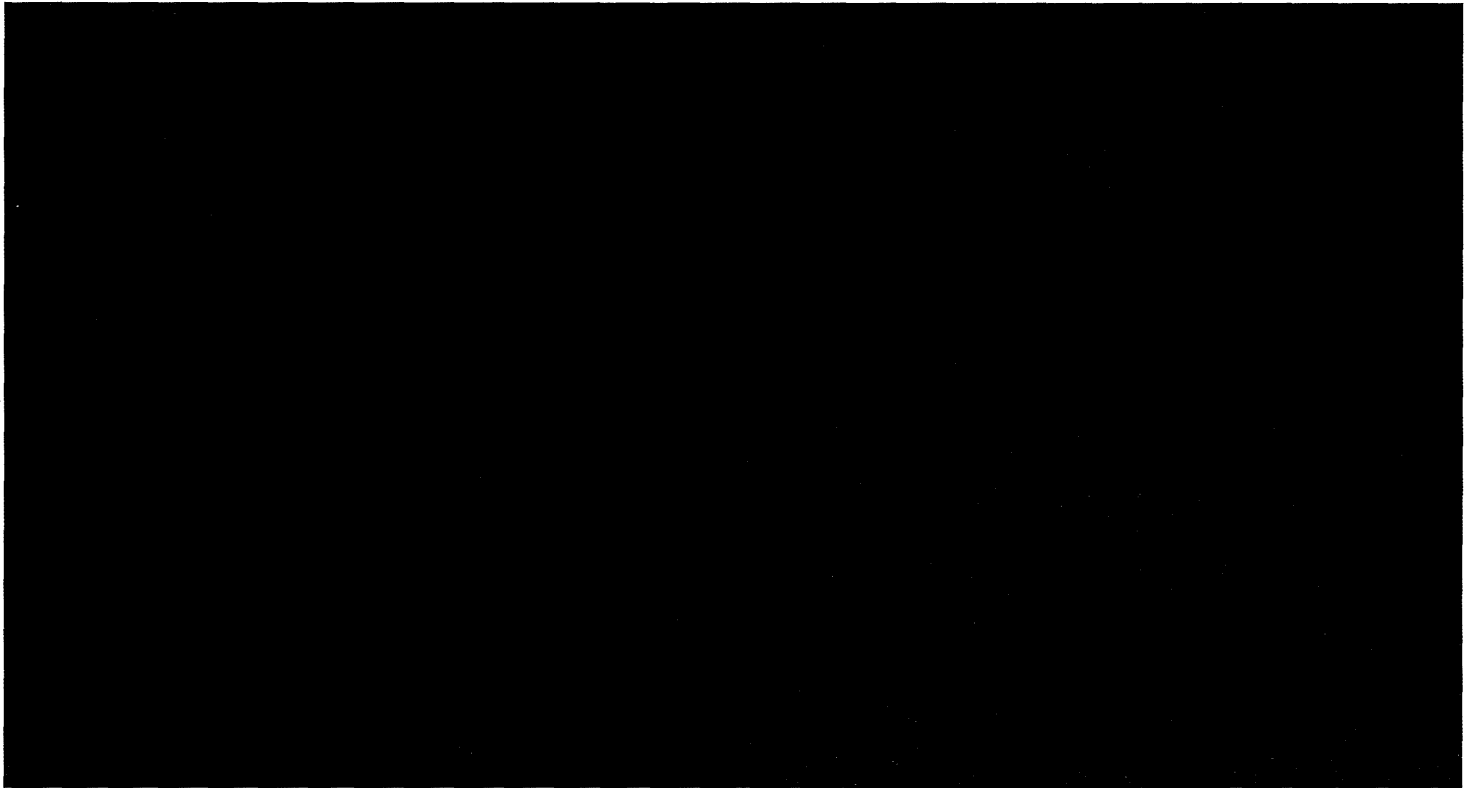
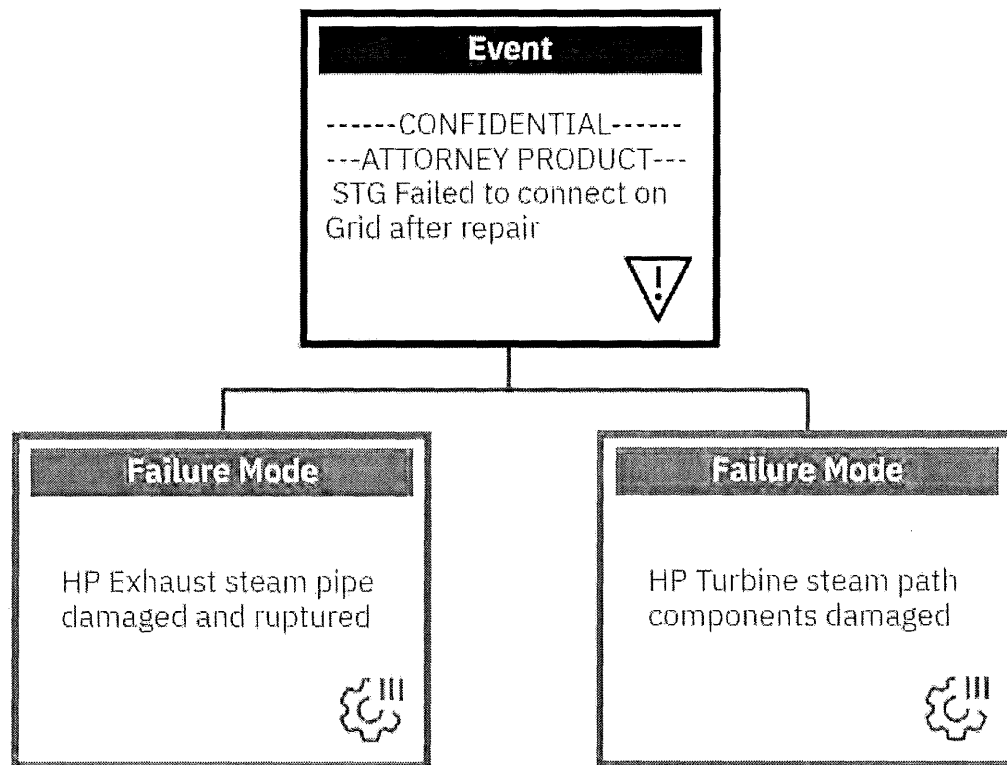
Figure 15, Trend data of GT2 Load and STG Turbine Speed (November 10th STG startup)

Figure 16, Comparison of Cold Startup curves (Actual vs Design)

PROACT® Logic Tree

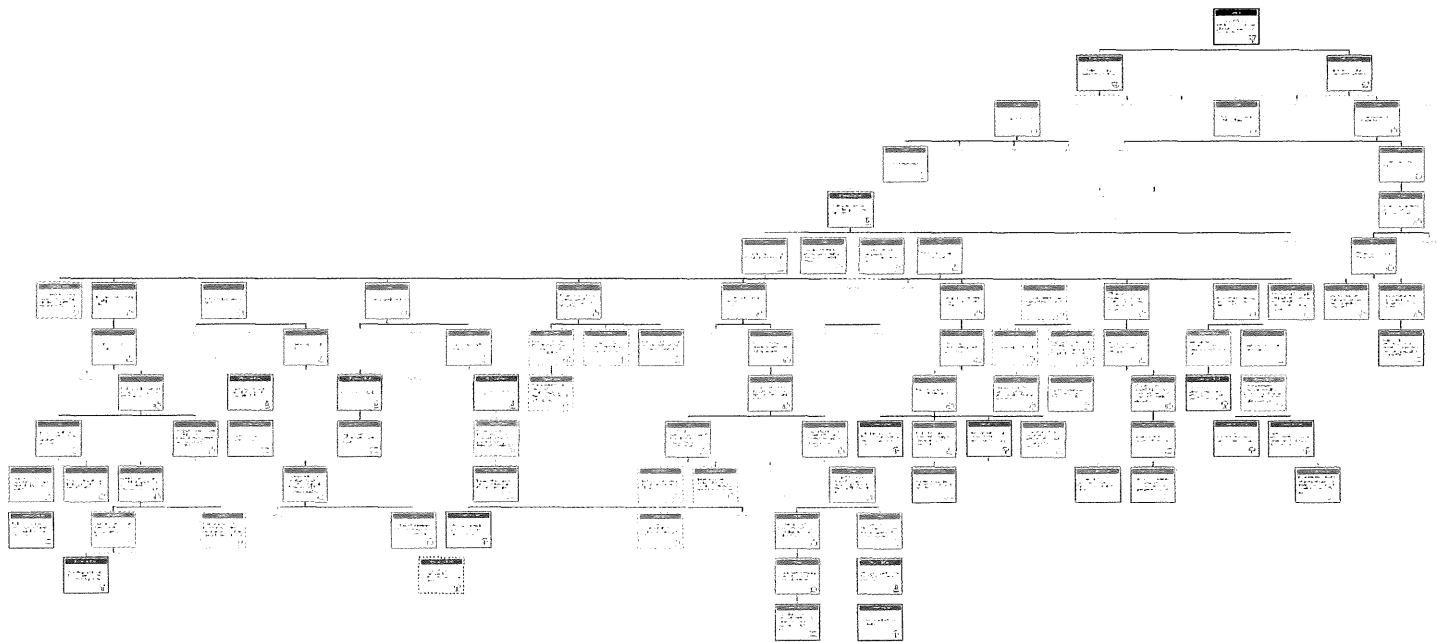
Any undesirable outcome is a result of a series of "cause-and-effect" relationships. The data provided by AES, in-person interviews and on-site visits, serve as proof (evidence) as to what did or what did not occur. A Logic Tree was utilized in the PROACT® application to graphically express the "cause-and-effect" relationships. In this approach, the top two levels of blocks represent the EVENT (Level 1) and the MODE (Level 2). From level-to-level the path represents a "cause-and-effect" relationship. These levels specifically represent the "undesirable outcomes" that did occur (facts only). From the MODE Level, the analysts do not know why they have occurred, just that they did occur. From this point the analysis becomes hypothetical and the analysts repeatedly ask the question "How Can?". As hypotheses are developed in this fashion, the evidence collected is used to verify what is true and what is not true. In this fashion, facts lead the analysis not assumptions. This process is reiterated until true root causes are uncovered; the reasons why people make decision errors that lead to undesirable outcome. Root causes originate from vulnerabilities in the organizational systems upon which employees depend to make informed decisions. These are called Latent Root Causes or Organizational Root Causes. Vulnerabilities in organizational systems lead to poor decisions being made by well-intentioned individuals. These decisions are referred to as Human Root Causes. Decision errors lead to the Physical Root Causes, or events or conditions that are visible. When the Latent Roots or Organizational System Roots are identified and addressed, the investigation becomes a true and effective Root Cause Analysis.

Top Box (problem definition)



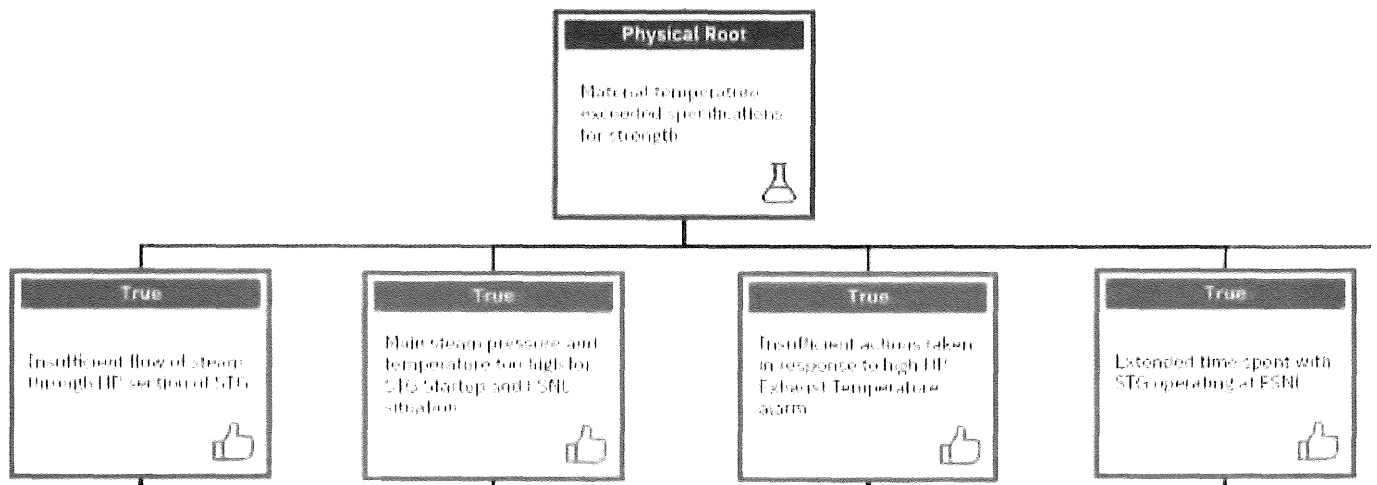
PROACT® Logic Tree Top Box

Entire Logic Tree



PROACT® Logic Tree

Logic Tree for material temperature exceeded specifications for strength.



Excerpt from PROACT® Logic Tree

Analysis Team Information

RCA Team Charter

To identify the root causes of the STG-1 generator failure to synchronize with grid and the damage to the generator field at the Eagle Valley power plant facility. This includes identifying deficiencies in, or lack of, management systems and oversight. Appropriate recommendations for root causes will be communicated to management for rapid resolution.

Analysis Critical Success Factors

- A cross-functional section of personnel/experts will participate in the analysis.
- All analysis hypotheses will be verified or disproven.
- Management agrees to fairly evaluate the analysis team's findings and recommendations.
- A disciplined RCA approach will be utilized.
- Use of an unbiased team facilitator who is an expert in the PROACT® RCA methodology.

Analysis Team Members

<u>Name</u>	<u>Role</u>	<u>Company</u>	<u>Title</u>
Mark Halbrook	Sponsor	AES	BOP Leader
Alex Halter	Principle Analyst	AES	Operations Leader
Eric Guilkey	Analyst	AES	Data Analyst
Holcombe Baird	Facilitator	Reliability Center, Inc.	Senior Reliability Consultant

Analysis Dates

Event Date: November 10, 2021

Analysis Start Date: November 12, 2021

Analysis Team Completion: January 31, 2022

Appendix A: Notes from the Initial Technical Review

HRSR Ramp Rate Control

In the Nooter Erikson Operation Training Manual N/E Training Manual-

During the startup from 11/8/2021 through 11/10/2021, all three of these systems did not operate correctly. First, the steam bypass system did not control correctly due to improper logic in the DCS. Second, it was decided to increase the loading of the gas turbine to 90MW. Third, the startup vent valves are not used in the startup procedure. These three failures contributed to the overheating of the HP turbine and the cold reheat piping.

HRH (IP Turbine) Bypass Valve



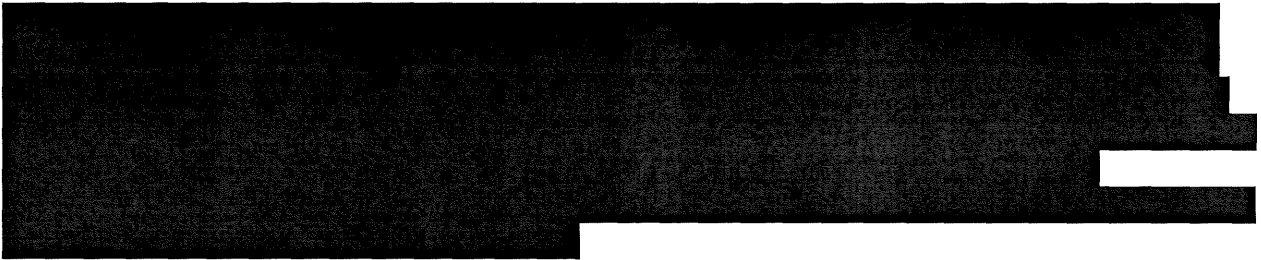
Control Narrative



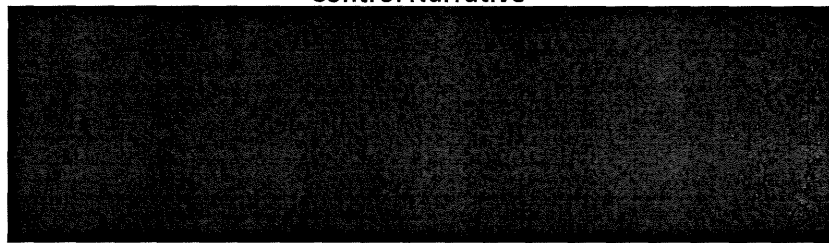
Actual DCS Logic



Table A.1



Control Narrative



Actual DCS Logic



Table A.2

MS (HP Turbine) Bypass Valve

[REDACTED]

[REDACTED]

[REDACTED]

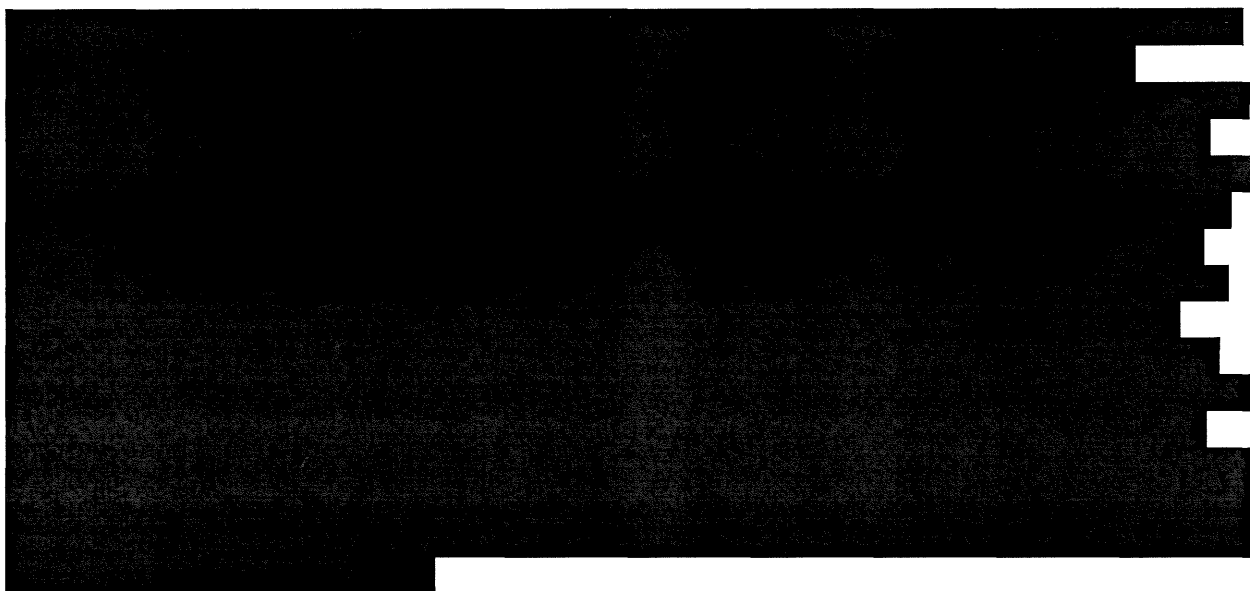
Gas Turbine Exhaust Temp Matching ST Temp

[REDACTED]

[REDACTED]

HRSG Startup Vent Valves

[REDACTED]

Steam Turbine High Inlet Temperature and Pressure During Startup**Toshiba TTIL**

Toshiba issued a Toshiba Technical Information Letter TAES-TTIL-KT112001X Revision 1 on February 11, 2021. The subject of the TTIL is "Improving Reliability for Turbine Bypass Start-u

**Startup Procedure**

The startup procedure used was 2x1 Cold Start OI-SRT02 Rev 09. However, when going through the documentation provided by plant personnel, the current version is Rev 13. The newest revision was changed on 11/19/2021.

Appendix B: Reference Documents

Prelim Operational Data review

Toshiba, November 12, 2021

Improving Reliability for Turbine Bypass Start-up

Toshiba Technical Information Letter, TAES-TTIL-KT112001X Revision 1, February 11, 2021,

Inspection of Steam Turbine Cold Reheat SF Piping System

Thielsch Engineering, Inc., November 2021

2x1 Cold Start Procedure, OI-STR02

Eagle Valley Generation Station, Revision 9, August 24, 2021

Steam Turbine Start Up with Turbine Bypass System

Toshiba Operations Manual, Section 7, Document # PCD-GMH-XUEG1-001 Rev.2

Turbine Bypass System Control Narrative

CB&I Control Narrative, Document # 152418-000-IC-SY-TB001, Rev. 1, Dated 5-24-2016

Appendix C: Contributors to Analysis Effort

Billy Hunt – IPL Operator (CRO)

Dave Haymond - IPL Operator (CRO)

Larry Bland – IPL Operator (Outside)

Steve Lambert – IPL Operator (TRO)

Tyler Norton – IPL Operator (Outside)

Gary Lucas – IPL Operator (TRO)

Doug Blackwell – IPL Operator (CRO)

Steve Durham – IPL Operator (TRO)

Ron Stiles – IPL DCS Technician

Jason Hoage – IPL Operations Leader

Brandon Berlin – IPL Maintenance Leader

Revision Log

<u>Rev. No.</u>	<u>Date</u>	<u>Comment</u>
0	April 28, 2022	Issued for Client Use
1	May 20, 2022	Page 17, Text edited to correct statement